

Superhydrophobic and oleophobic surfaces for sustainable medical textiles

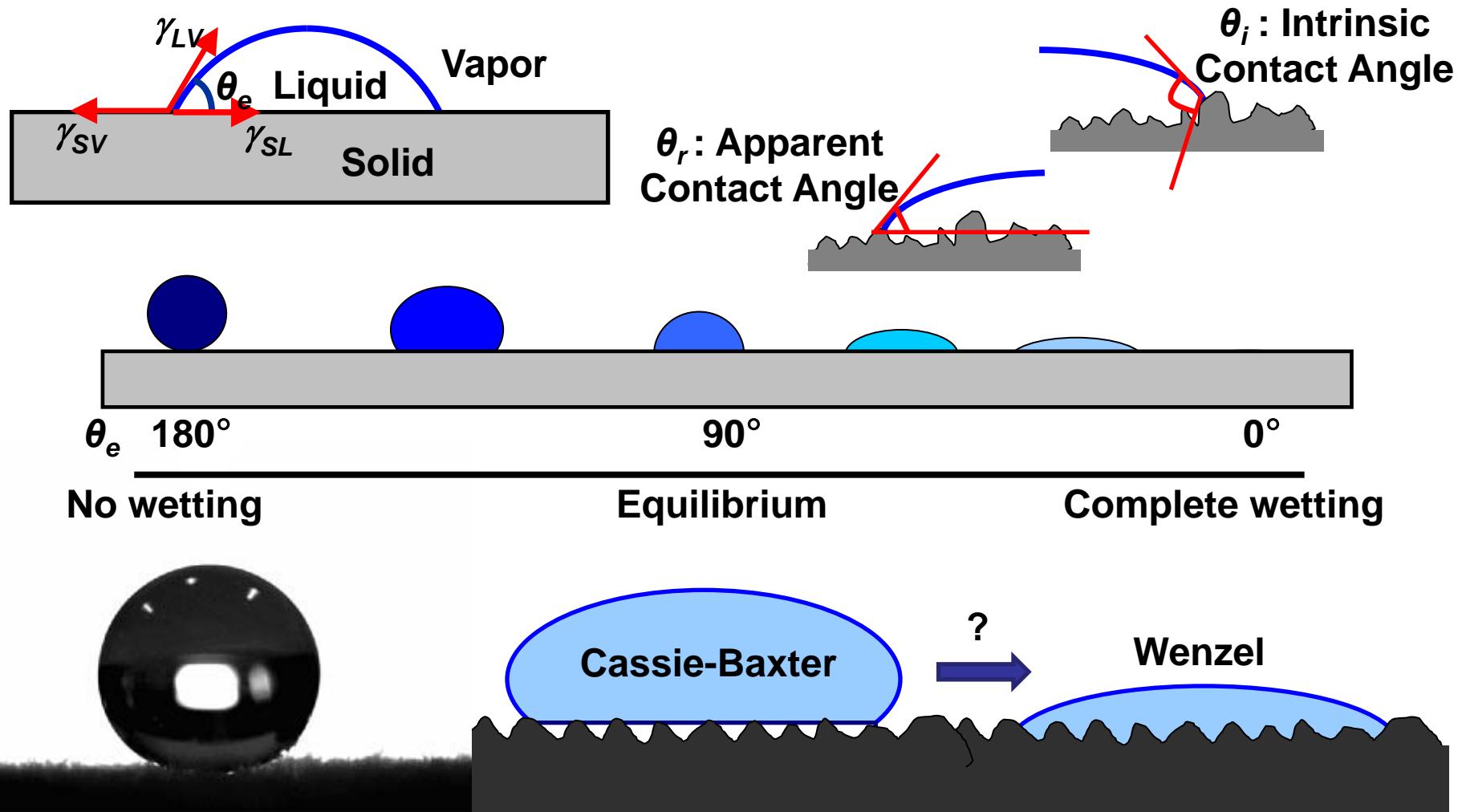
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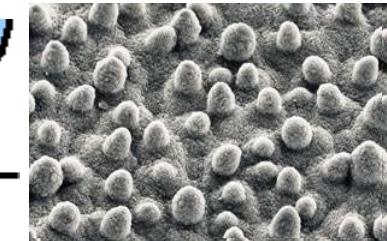
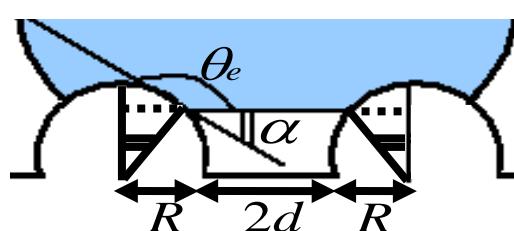
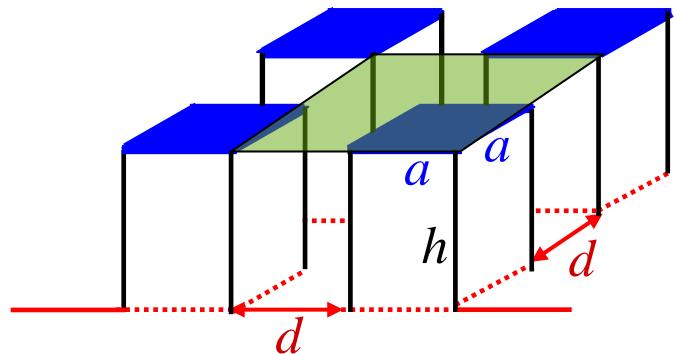
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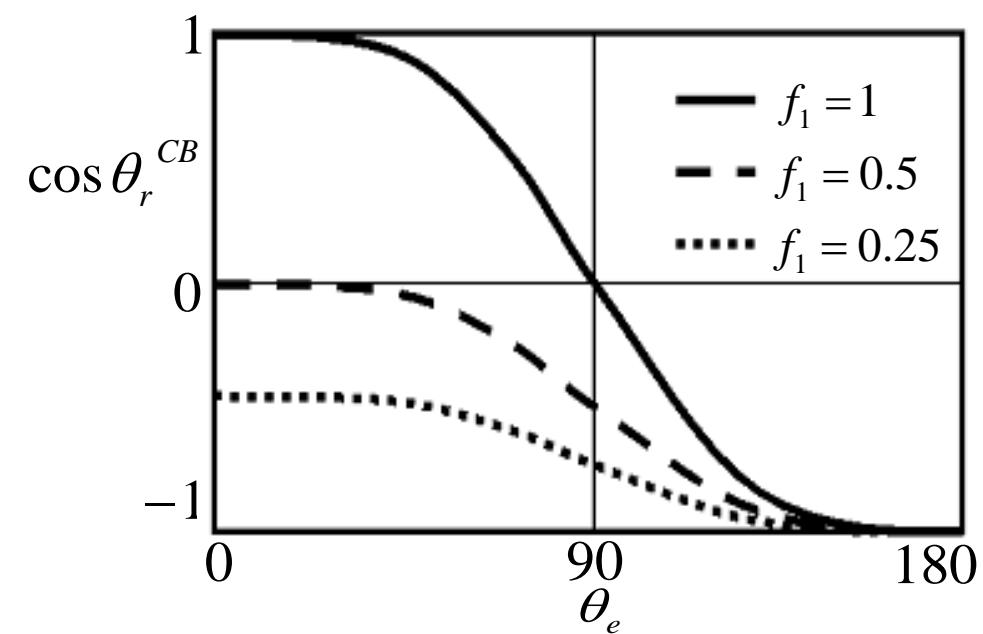
Contact Angle and Wetting Behavior



Design of Cassie Baxter Surface

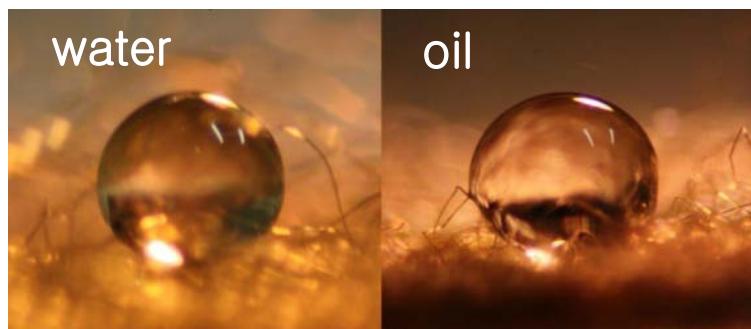


$$\cos \theta_r^{CB} = f_1 \cos \theta_e - f_2$$

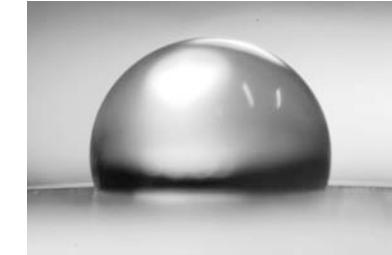
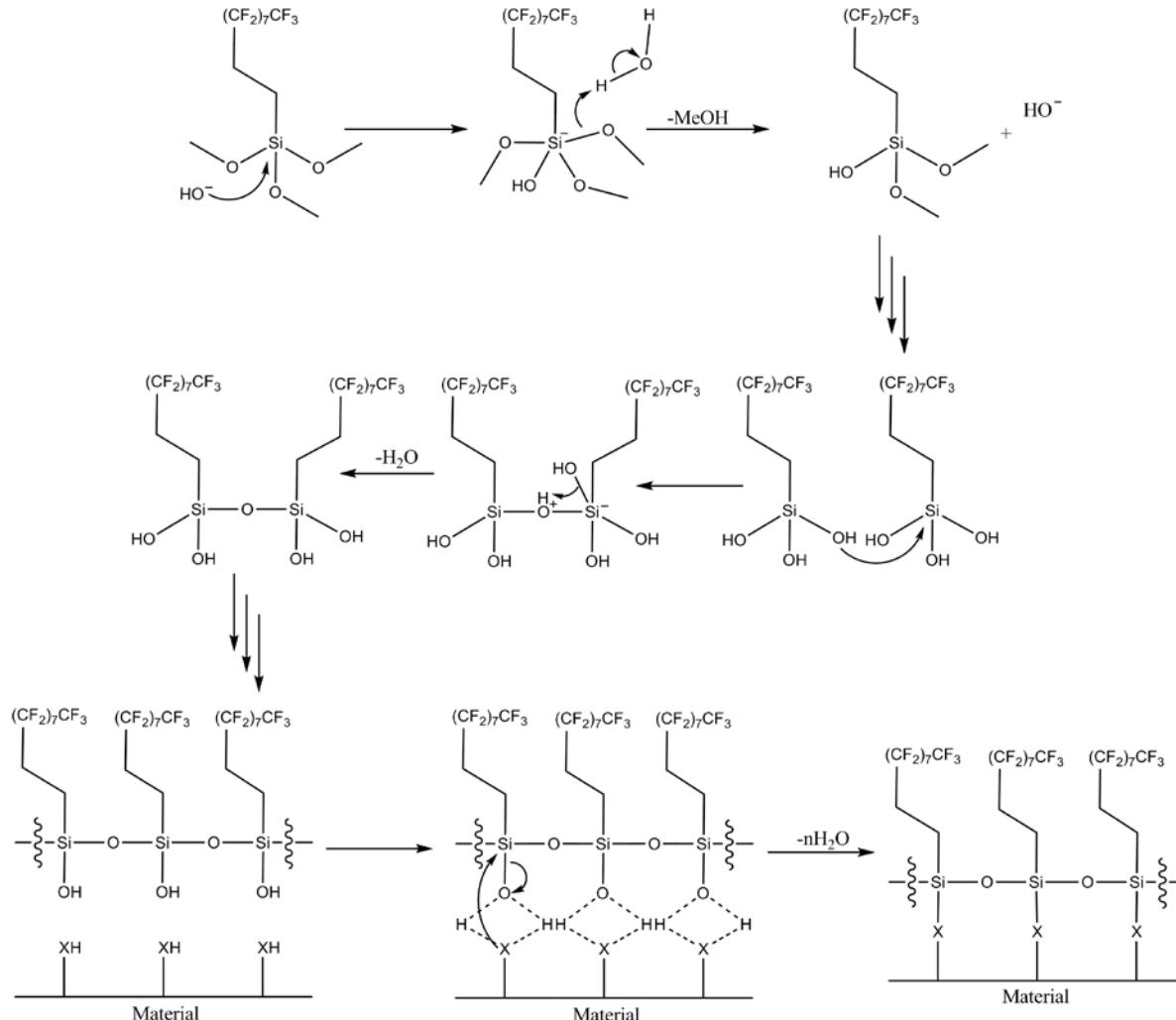


$$f_1 = \frac{\text{Area in contact with liquid}}{\text{Projected area}} = \frac{R\alpha}{R+d}$$

$$f_2 = \frac{\text{Area in contact with air}}{\text{Projected area}} = \frac{(R+d)-R \sin \alpha}{(R+d)}$$



Chemical Modification with F-silane through Microwave Reaction

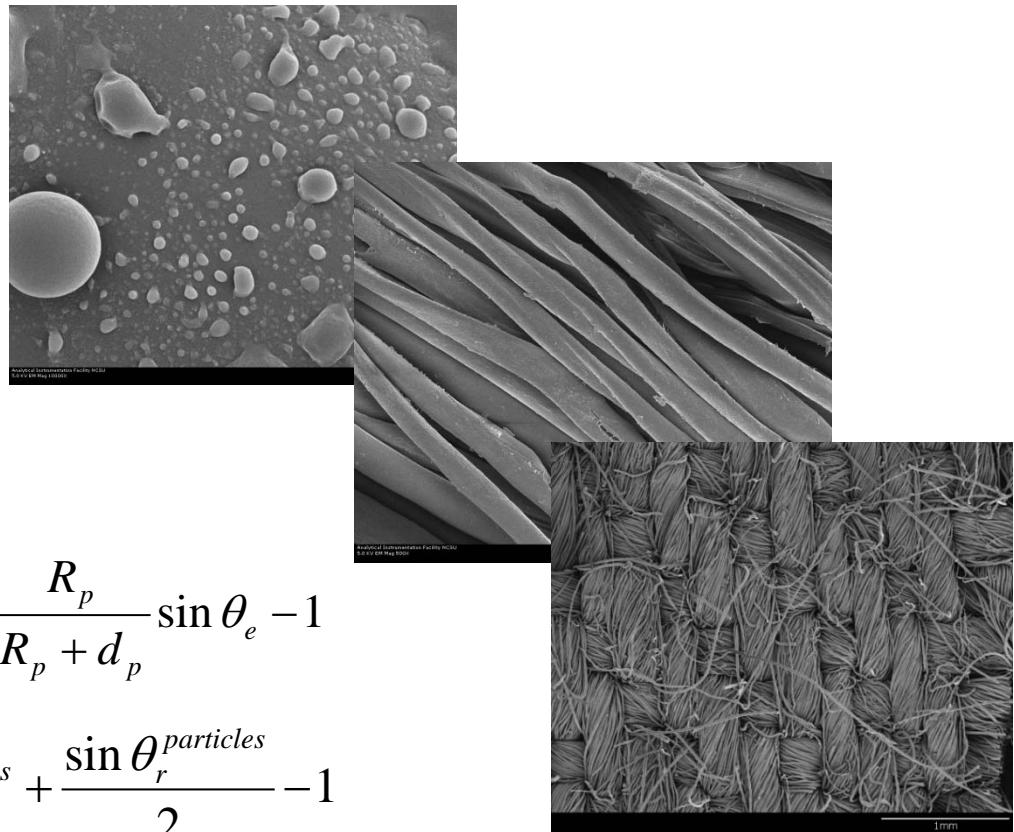
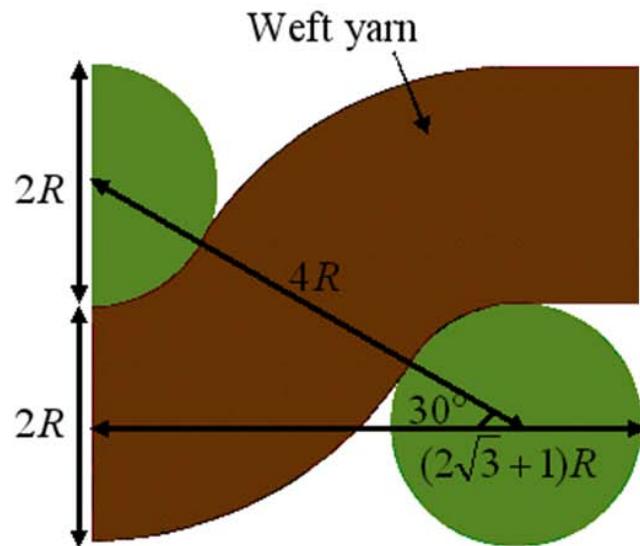


Water on
modified nylon



Dodecane on
modified nylon

Geographical Modification I – NyCo Multifilament Woven Fabric

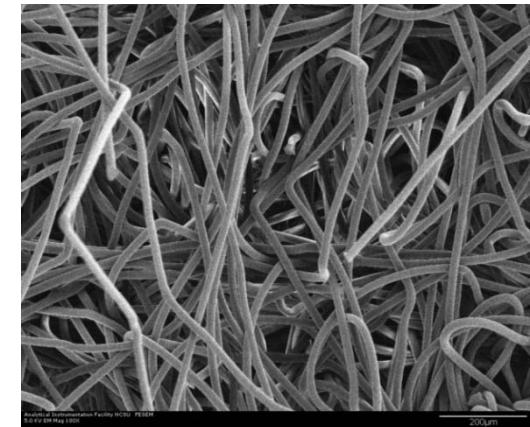
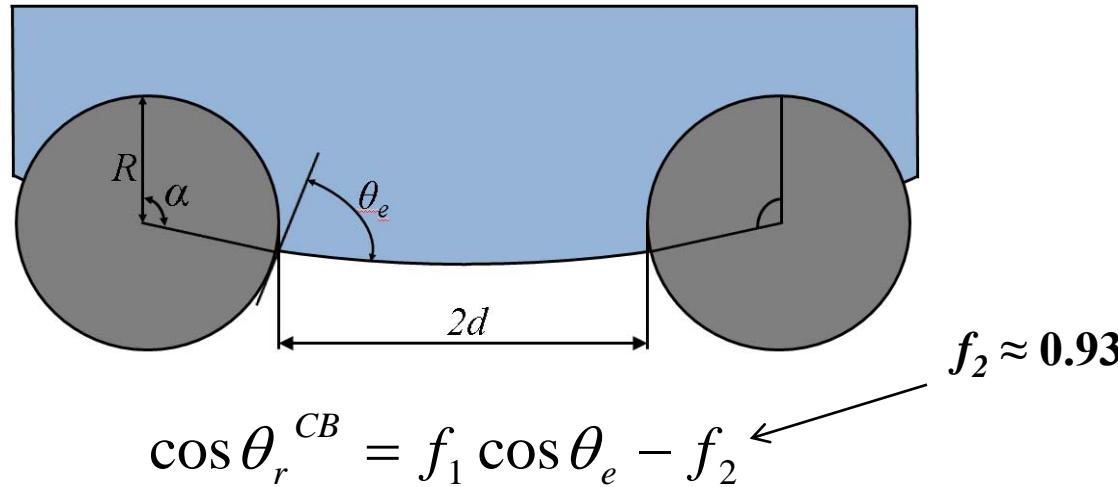


$$\cos \theta_r^{particles} = \frac{R_p}{R_p + d_p} (\pi - \theta_e) \cos \theta_e + \frac{R_p}{R_p + d_p} \sin \theta_e - 1$$

$$\cos \theta_r^{multifilament} = \frac{\pi - \theta_r^{particles}}{2} \cos \theta_r^{particles} + \frac{\sin \theta_r^{particles}}{2} - 1$$

$$\cos \theta_r^{NyCo} = \frac{4(\pi - \theta_r^{Multifilament}) + 1}{2\sqrt{3} + 1} \cos \theta_r^{Multifilament} + \frac{1 + 4 \sin \theta_r^{Multifilament}}{2\sqrt{3} + 1} - 1$$

Geographical Modification II – Nylon Hydroentangled Nonwoven Fabric

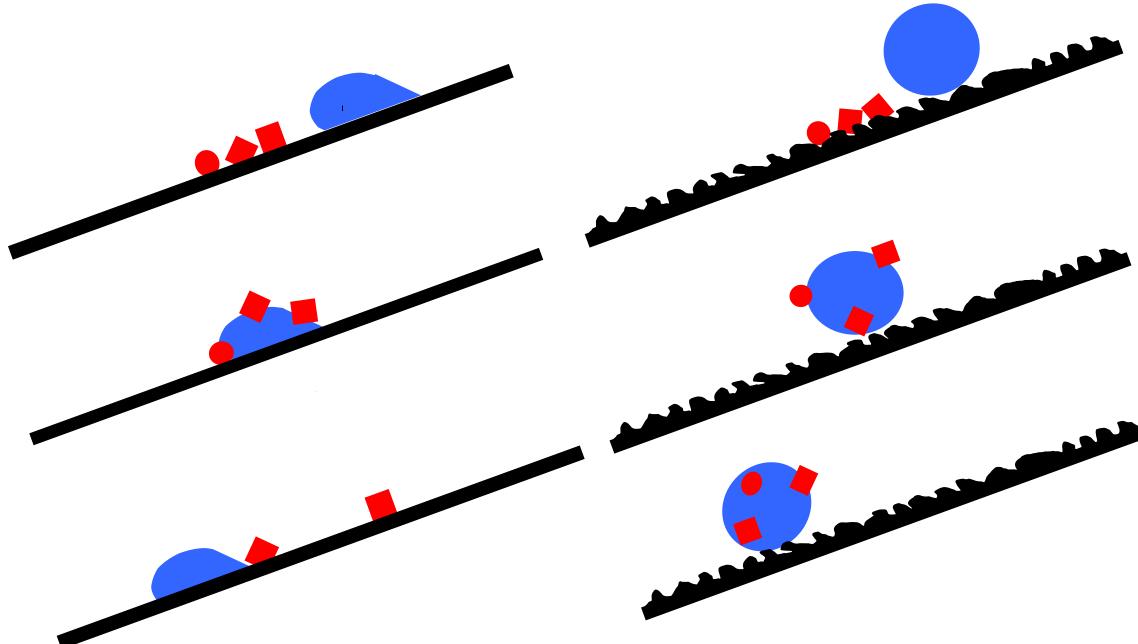


$$\cos \theta_r^{CB} = \frac{R(\pi - \theta_e)}{d + R} \cos \theta_e + \frac{R}{d + R} \sin \theta_e - 1 \xrightarrow{\substack{R \approx 10 \text{ } \mu\text{m} \\ 78^\circ \leq \theta_{e-dodecane} \leq 81^\circ}} d \leq 131 \text{ } \mu\text{m}$$

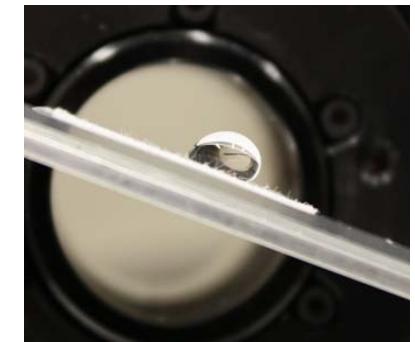
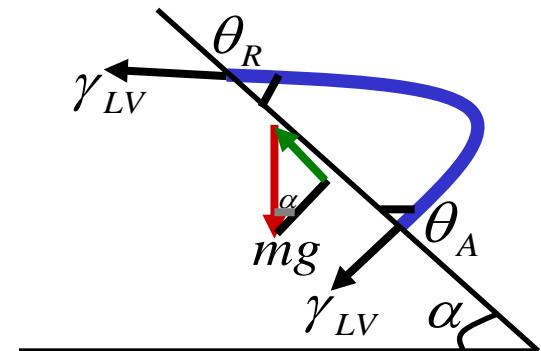
$155^\circ \leq \theta_{r-dodecane} \leq 156^\circ$

Superhydrophobicity vs Superoleophobicity

$$mg \sin \alpha = \gamma_{LV}(\cos \theta_R - \cos \theta_A)$$



Self-cleaning effect by superhydrophobicity.
(Source: Barthlott, W., Neihuis, C., *Planta*, 1997, 202, 1.)



Roll-off Angles and Contact Angle Hysteresis

- Wenzel Model

$$\cos \theta_e^W = r \cos \theta_e$$

$$G_e^W = \frac{r \sin \theta_e}{\sin \theta_e^W}$$

$$\Delta \theta_H^W = G_e^W \Delta \theta_H$$

- Cassie-Baxter Model

$$\cos \theta_e^{CB} = \Phi_s (\cos \theta_e + 1) - 1$$

$$G_e^{CB} = \frac{\Phi_s \sin \theta_e}{\sin \theta_e^{CB}}$$

$$\Delta \theta_H^{CB} = G_e^{CB} \Delta \theta_H$$

- Numerical Example

$\theta_e = 120^\circ$, $\theta_h = 15^\circ$, $a = 0.01\text{mm}$,
 $d = 0.2\text{mm}$, and $h = 1\text{mm}$

In Wenzel model,

$$r = 1.9$$

$$\theta_e^W = 162^\circ$$

$$G_e^W = 5.32$$

$$\text{and } \theta_h^W = 80^\circ$$

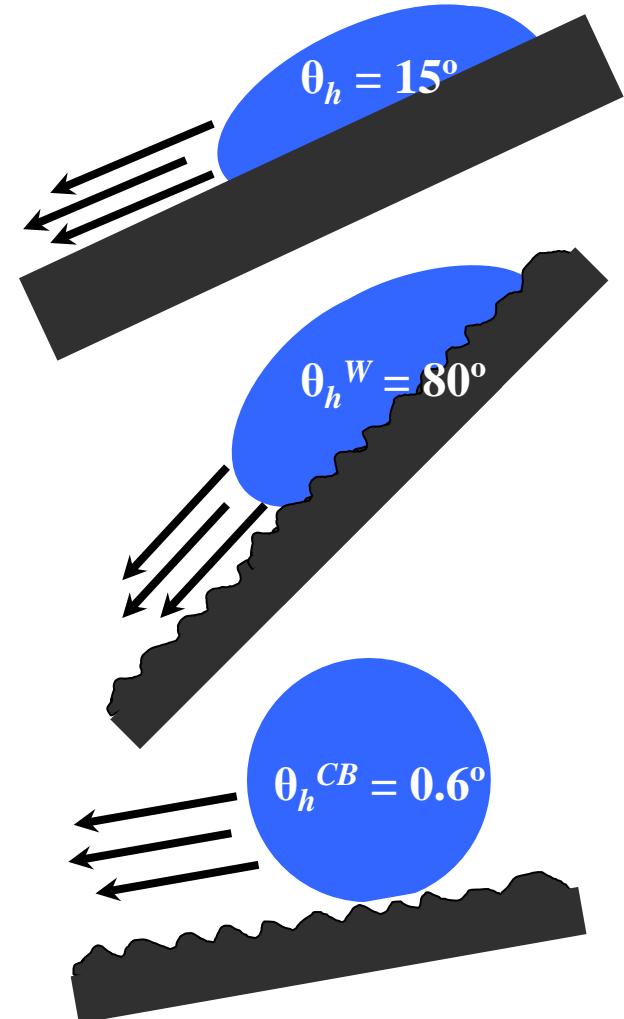
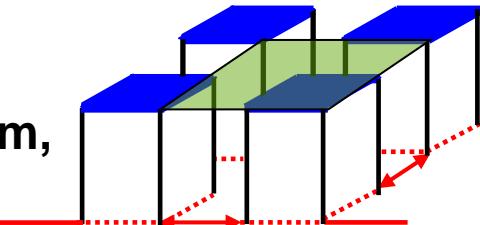
In Cassie-Baxter model,

$$\Phi_s = 0.0023$$

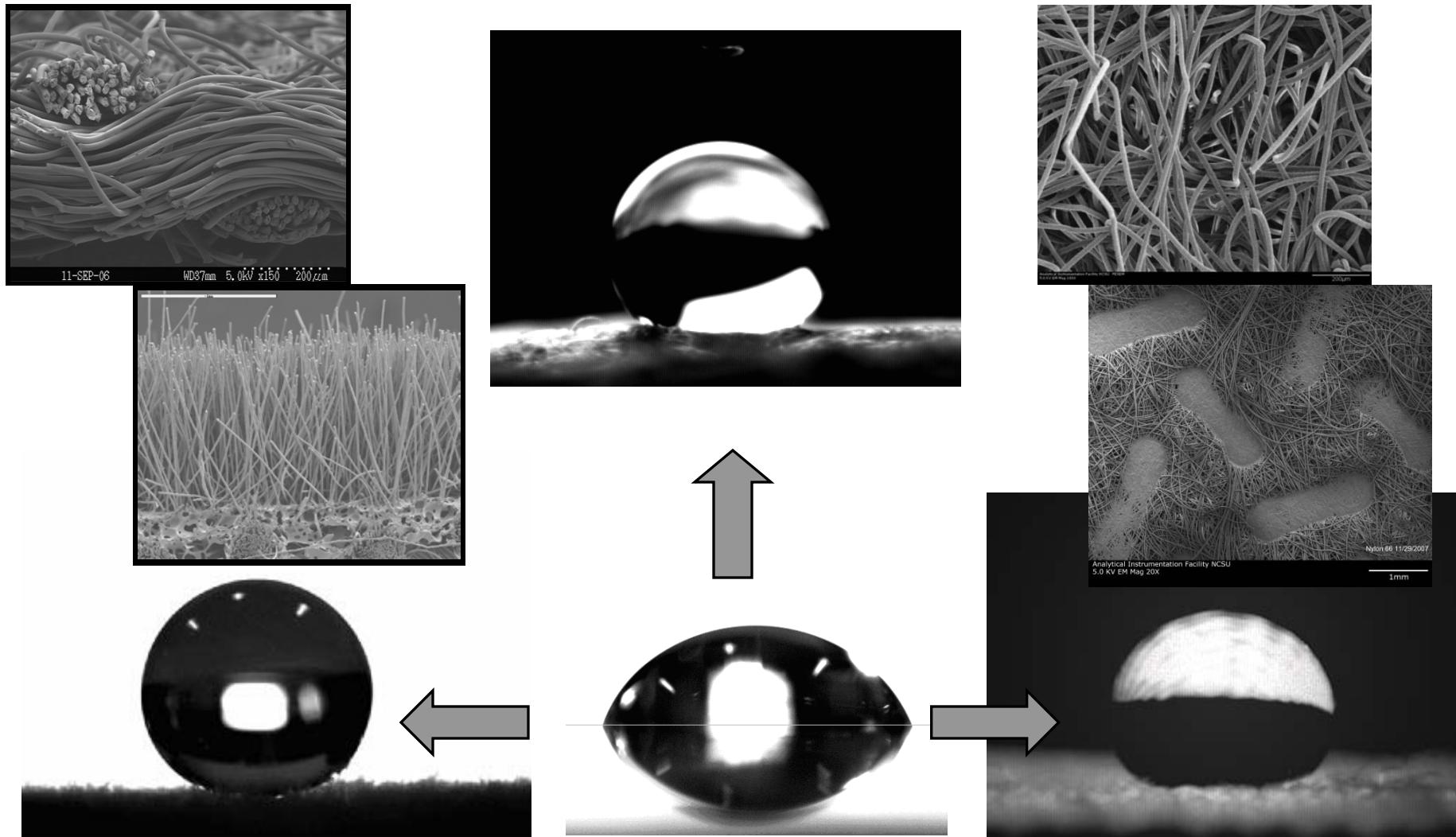
$$\theta_e^{CB} = 177^\circ$$

$$G_e^{CB} = 0.04$$

$$\text{and } \theta_h^{CB} = 0.6^\circ$$



Conclusion



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Thank you.

